

LAMPIRAN

1. COS Ø

- φ : phase angle between voltage
- Incandescent lighting: $\cos \varphi = 1$
- Led lighting: $\cos \varphi > 0.9$
- Fluorescent with electronic ballast
- Motor power:
 - At start-up: $\cos \varphi = 0.35$
 - In normal service: $\cos \varphi = 0.8$

2. KAPASITAS TRANSFORMATOR

Apparent power kVA	In (A)	
	237 V	410 V
100	244	141
160	390	225
250	609	352
315	767	444
400	974	563
500	1218	704
630	1535	887
800	1949	1127
1000	2436	1408
1250	3045	1760
1600	3898	2253
2000	4872	2816
2500	6090	3520
3150	7673	4436

Fig. A15: Standard apparent powers for MV/LV transformers and related nominal output currents

3. KAPASITAS GENERATOR

Determining the number of back-up generator units is in line with the same criteria as determining the number of transformers, as well as taking account of economic and availability considerations (redundancy, start-up reliability, maintenance facility).

Determining the generator apparent power, depends on:

- installation power demand of loads to be supplied,
- transient constraints that can occur by motors inrush current for example.

4. TEGANGAN JATUH

3.1 Maximum voltage drop limit

Maximum allowable voltage-drop vary from one country to another. Typical values for LV installations are given below in Figure G25.

Type of installations	Lighting circuits	Other uses (heating and power)
A low-voltage service connection from a LV public power distribution network	3 %	5 %
Consumers MV/LV substation supplied from a public distribution MV system	6 %	8 %

Fig. G25: Maximum voltage-drop between the service-connection point and the point of utilization (IEC60364-5-52 table G.52.1)

These voltage-drop limits refer to normal steady-state operating conditions and do not apply at times of motor starting, simultaneous switching (by chance) of several loads, etc. as mentioned in Chapter A Sub-clause 4.3 (diversity and utilization factors, etc.). When voltage drops exceed the values shown in Figure G25, larger cables (wires) must be used to correct the condition.

The value of 8 %, while permitted, can lead to problems for motor loads; for example:

- In general, satisfactory motor performance requires a voltage within $\pm 5\%$ of its rated nominal value in steady-state operation,
- Starting current of a motor can be 5 to 7 times its full-load value (or even higher). If an 8 % voltage drop occurs at full-load current, then a drop of 40 % or more will occur during start-up. In such conditions the motor will either:
 - Stall (i.e. remain stationary due to insufficient torque to overcome the load torque) with consequent over-heating and eventual trip-out
 - Or accelerate very slowly, so that the heavy current loading (with possibly undesirable low-voltage effects on other equipment) will continue beyond the normal start-up period
- Finally an 8 % voltage drop represents a continuous power loss, which, for continuous loads will be a significant waste of (metered) energy. For these reasons it is recommended that the maximum value of 8 % in steady operating conditions should not be reached on circuits which are sensitive to under-voltage problems (see Fig. G26).

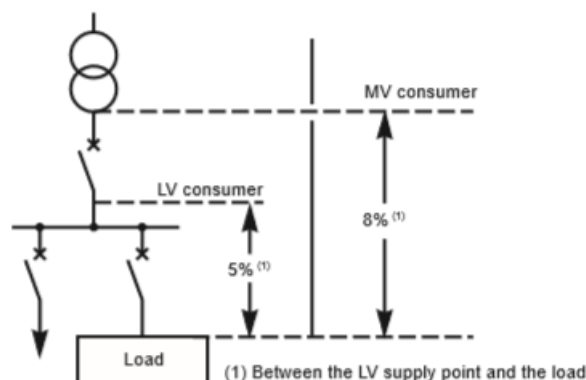


Fig. G26: Maximum voltage drop

5. ARUS HUBUNG SINGKAT

4.1 Short-circuit current at the secondary terminals of a MV/LV distribution transformer

The case of one transformer

■ In a simplified approach, the impedance of the MV system is assumed to be

negligibly small, so that: $I_{sc} = \frac{I_n \times 100}{U_{sc}}$ where $I_n = \frac{S \times 10^3}{U_{20}\sqrt{3}}$ and:

S = kVA rating of the transformer

U_{20} = phase-to-phase secondary volts on open circuit

I_n = nominal current in amps

I_{sc} = short-circuit fault current in amps

U_{sc} = short-circuit impedance voltage of the transformer in %.

Typical values of U_{sc} for distribution transformers are given in Figure G31.

Transformer rating (kVA)	U _{sc} in %	
	Oil-immersed	Cast-resin dry type
50 to 750	4	6
800 to 3200	6	6

Fig. G31: Typical values of U_{sc} for different kVA ratings of transformers with MV windings ≤ 20 kV

6. KAPASITOR BANK

For 2-part tariffs based partly on a declared value of kVA, Figure L17 allows determination of the kvar of compensation required to reduce the value of kVA declared, and to avoid exceeding it

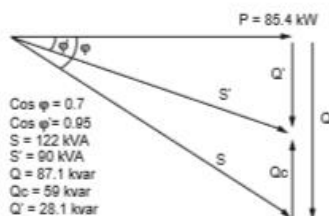


Fig. L16 : Reduction of declared maximum kVA by power-factor improvement

(1) In the billing period, during the hours for which reactive energy is charged for the case considered above:

$$Q_c = \frac{15,000 \text{ kvarh}}{220 \text{ h}} = 73 \text{ kvar}$$

5.4 Method based on reduction of declared maximum apparent power (kVA)

For consumers whose tariffs are based on a fixed charge per kVA declared, plus a charge per kWh consumed, it is evident that a reduction in declared kVA would be beneficial. The diagram of Figure L16 shows that as the power factor improves, the kVA value diminishes for a given value of kW (P). The improvement of the power factor is aimed at (apart from other advantages previously mentioned) reducing the declared level and never exceeding it, thereby avoiding the payment of an excessive price per kVA during the periods of excess, and/or tripping of the the main circuit-breaker. Figure L15 (previous page) indicates the value of kvar of compensation per kW of load, required to improve from one value of power factor to another.

Example:

A supermarket has a declared load of 122 kVA at a power factor of 0.7 lagging, i.e. an active-power load of 85.4 kW. The particular contract for this consumer was based on stepped values of declared kVA (in steps of 6 kVA up to 108 kVA, and 12 kVA steps above that value, this is a common feature in many types of two-part tariff). In the case being considered, the consumer was billed on the basis of 132 kVA. Referring to Figure L15, it can be seen that a 60 kvar bank of capacitors will improve the power factor of the load from 0.7 to 0.95 ($0.691 \times 85.4 = 59 \text{ kvar}$ in the figure). The declared value of kVA will then be $\frac{85.4}{0.95} = 90 \text{ kVA}$, i.e. an improvement of 30%.

7. CIRCUIT BREAKER

510.5.8.3 Syarat bagi sarana pemutus

510.5.8.3.1 Sarana pemutus harus dapat memutuskan hubungan antara motor serta kendali dan semua konduktor suplai yang tak dibumikan, dan harus didesain sedemikian sehingga tidak ada kutub yang dapat dioperasikan tersendiri.

510.5.8.3.2 Sarana pemutus harus dapat menunjukkan dengan jelas apakah sarana tersebut pada kedudukan terbuka atau tertutup.

510.5.8.3.3 Sarana pemutus harus mempunyai kemampuan arus sekurang-kurangnya 115 % dari arus beban penuh motor.

510.5.8.3.4 Sarana pemutus yang melayani beberapa motor atau melayani motor dan beban lainnya, harus mempunyai kemampuan arus sekurang-kurangnya 115% dari jumlah arus beban pada keadaan beban penuh.

8. KABEL TENAGA (FEEDER)

510.5.4.2 Penggunaan

510.5.4.2.1 Dalam lingkungan dengan gas, uap, atau debu yang mudah terbakar atau mudah meledak, setiap motor magun, harus diproteksi terhadap beban lebih.

510.5.4.2.2 Setiap motor trifase atau motor berdaya pengenal satu daya kuda atau lebih, yang magun dan dijalankan tanpa pengawasan, harus diproteksi terhadap beban lebih.

510.5.4.3 Gawai proteksi beban lebih motor terdiri atas GPAL dan GPHP.

Arus pengenal GPAL motor sekurang-kurangnya 110% - 115% arus pengenal motor.

Arus pengenal GPHP harus dikoordinasikan dengan KHA kabel.

KHA kabel (I_2) sesuai 510.5.3.1 adalah 125 % arus pengenal beban penuh motor (I_B).

Menurut persamaan pada Ayat 433.1 maka arus pengenal GPHP harus $\leq I_2$, biasanya nilainya di antara I_B dan I_L .

9. UPS/CDPK

8.27.6.5 Pengujian berkala

8.27.6.5.1 Untuk mempertahankan tingkat keamanan yang tinggi dari seluruh instalasi haruslah dilakukan pengujian berkala terhadap instalasi yang digunakan.

8.27.6.5.2 Hasil pengujian harus dicatat dalam buku uji sesuai dengan 8.27.6.1.

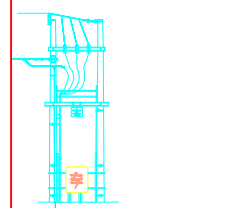
8.27.6.5.3 Pengujian berkala dilaksanakan sebagai berikut:

- Pengujian sesuai dengan 8.27.6 harus dilakukan oleh orang juru sekurang-kurangnya setahun sekali.
- Pengujian monitor insulasi dan sakelar proteksi arus sisa harus dilakukan oleh petugas yang ditunjuk dengan menekan tombol uji sekurang-kurangnya setengah tahun sekali.
- Uji coba CDPK harus dilakukan dengan pembebanan sekurang-kurangnya 50 % daya nominal : selama 15 menit untuk catu daya statis dan konverter berputar dan 60 menit

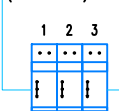
ESTIMASI KEBUTUHAN BEBAN LISTRIK :

NAMA GEDUNG	LUASAN TOTAL GEDUNG (GROSS FLOOR AREA)	FUNGSI BANGUNAN	ESTIMASI LISTRIK PER METER PERSEGI (VA/m ²)	TOTAL KEBUTUHAN LISTRIK (KVA)
GEDUNG MEDIK SENTRAL (TAHAP 1)	7455 m ²	IGD, RADIOLOGI, FARMASI, ADMISI TERPADU, KOMERSIAL, KLINIK, LABORATORIUM, CSSD, ICU, HCU, OK	75	559
GEDUNG EKSIKSTING				197
			TOTAL	756

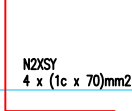
TAMBAH DAYA PLN
 DATA : 1.110 KVA
 JENIS : TEGANGAN MENENGAH



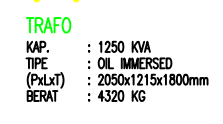
N2XSEBY 3x70mm²
 + N2XSY 70mm²
 (LINGKUP PLN)



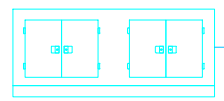
PANEL TM PLN 3 CELL (LINGKUP PLN)
 TIPE : FREE STANDING
 (PxLxT) : 1800 x 1000 x 1600 mm
 BERAT : 950 KG



PANEL TM PELANGGAN 2 CELL (LINGKUP PELANGGAN)
 1. CIRCUIT BREAKER + LIGHTNING ARRESTER
 2. LBS + FUSE
 TIPE : FREE STANDING
 (PxLxT) : 1350 x 1000 x 1600 mm
 BERAT : 700 KG



TRAFO
 KAP. : 1250 KVA
 TIPE : OIL IMMERSIED
 (PxLxT) : 2050x1215x1800mm
 BERAT : 4320 KG

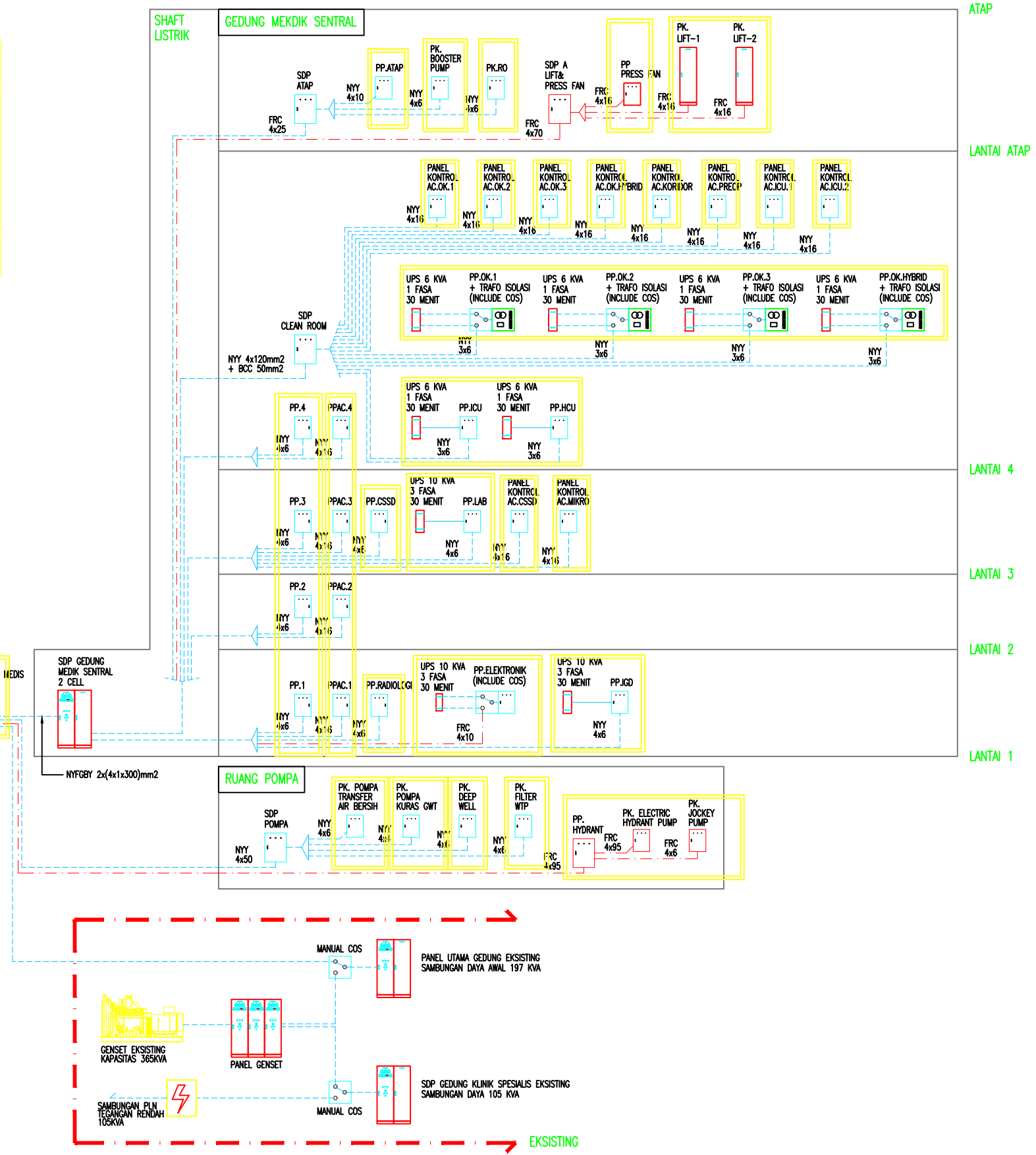
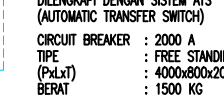


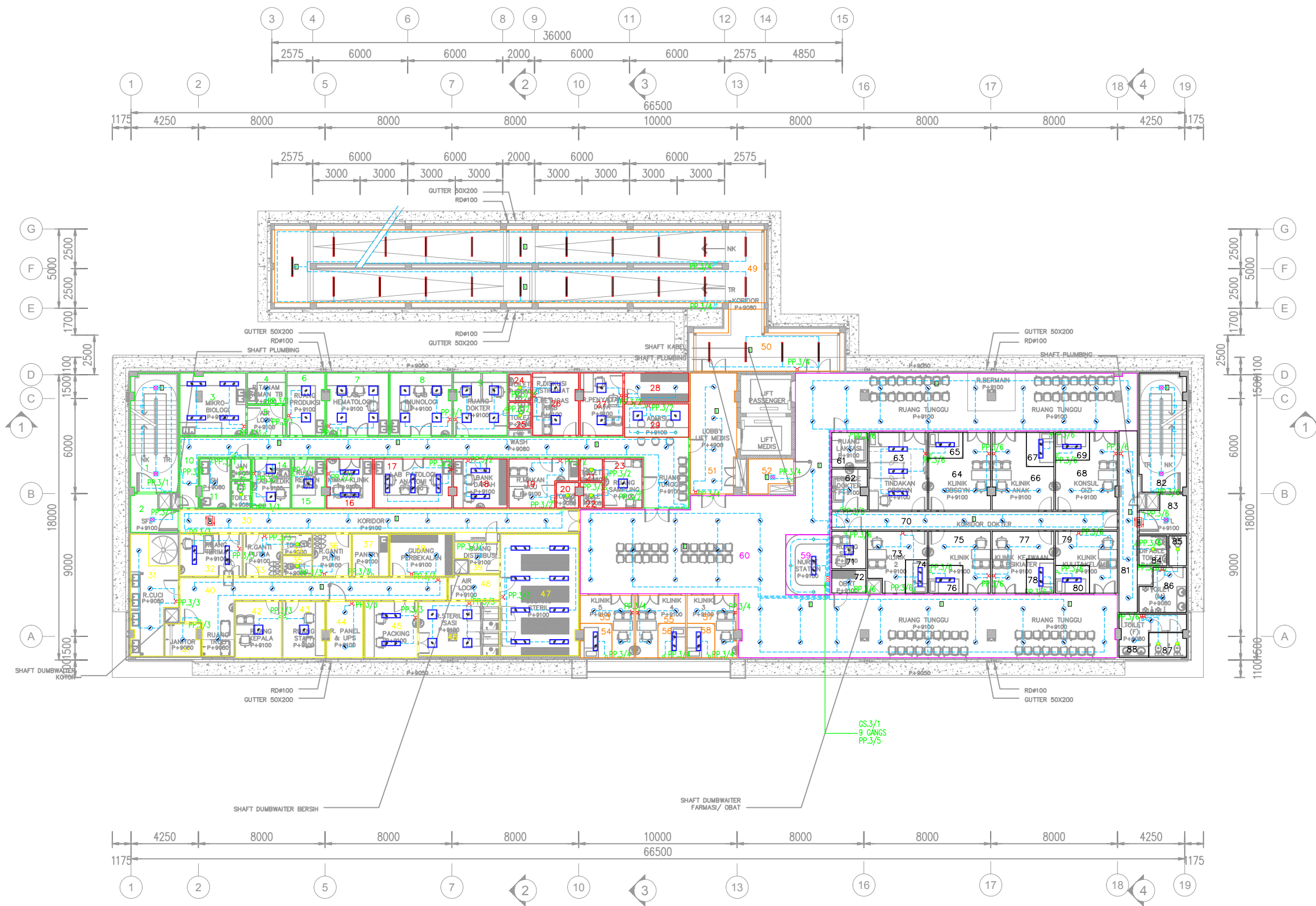
GENSET
 KAP. : 1250 KVA - PRIME
 TIPE : SILENT
 (PxLxT) : 6100 x 2350 x 2580 mm
 BERAT : 9500 KG

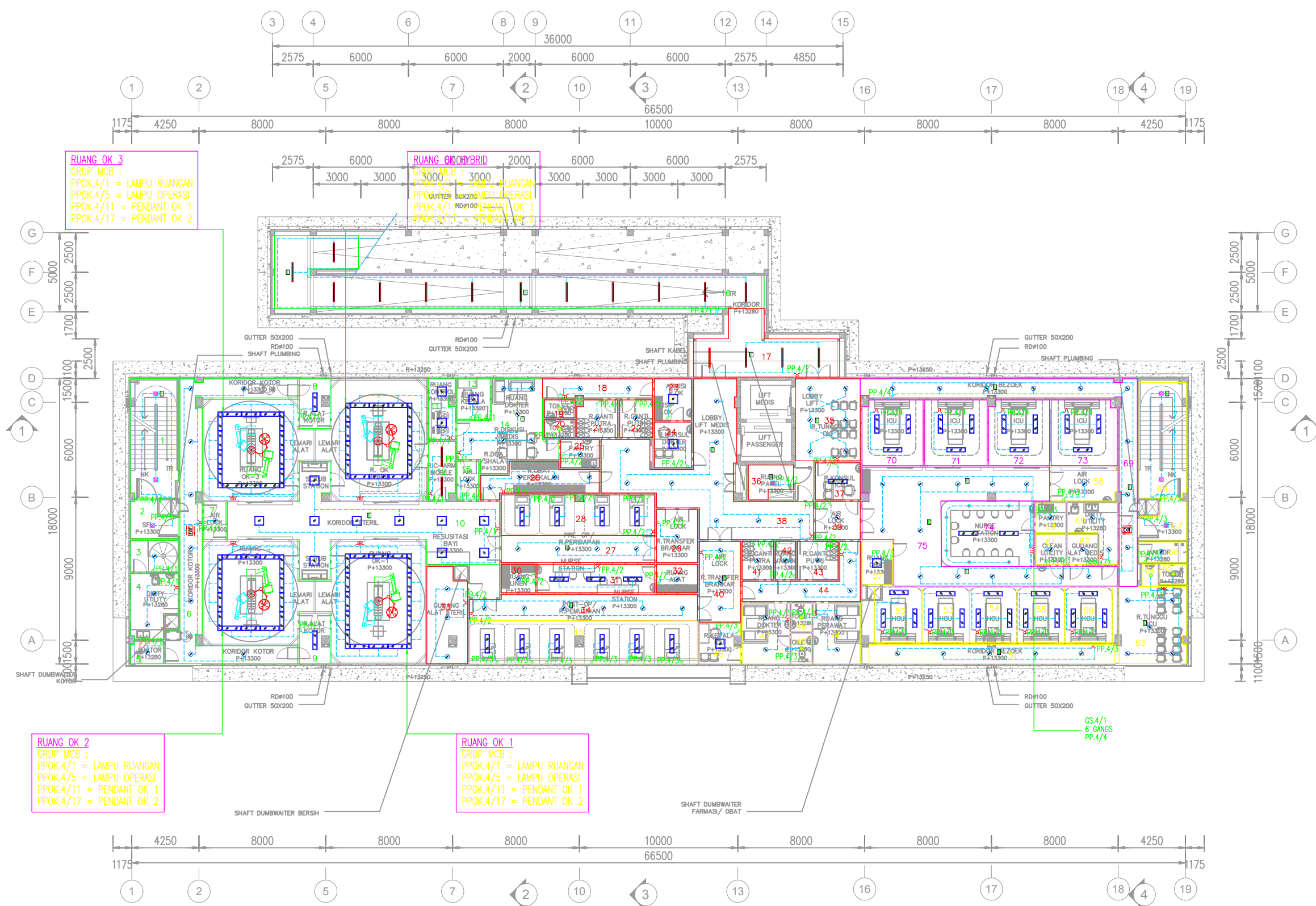
ACTIVE HARMONIC FILTER



LVMDP 5 CELL
 DILENGKAPI DENGAN SISTEM ATS (AUTOMATIC TRANSFER SWITCH)
 CIRCUIT BREAKER : 2000 A
 TIPE : FREE STANDING
 (PxLxT) : 4000x800x2000 mm
 BERAT : 1500 KG







RUANG OK 3
 GRUP MCB :
 PPOK.4/1 = LAMPU RUANGAN
 PPOK.4/5 = LAMPU OPERASI
 PPOK.4/11 = PENDANT OK 1
 PPOK.4/17 = PENDANT OK 2

RUANG OK 000BYRID
 GRUP MCB :
 PPOK.4/1 = LAMPU RUANGAN
 PPOK.4/5 = LAMPU OPERASI
 PPOK.4/11 = PENDANT OK 1
 PPOK.4/17 = PENDANT OK 2

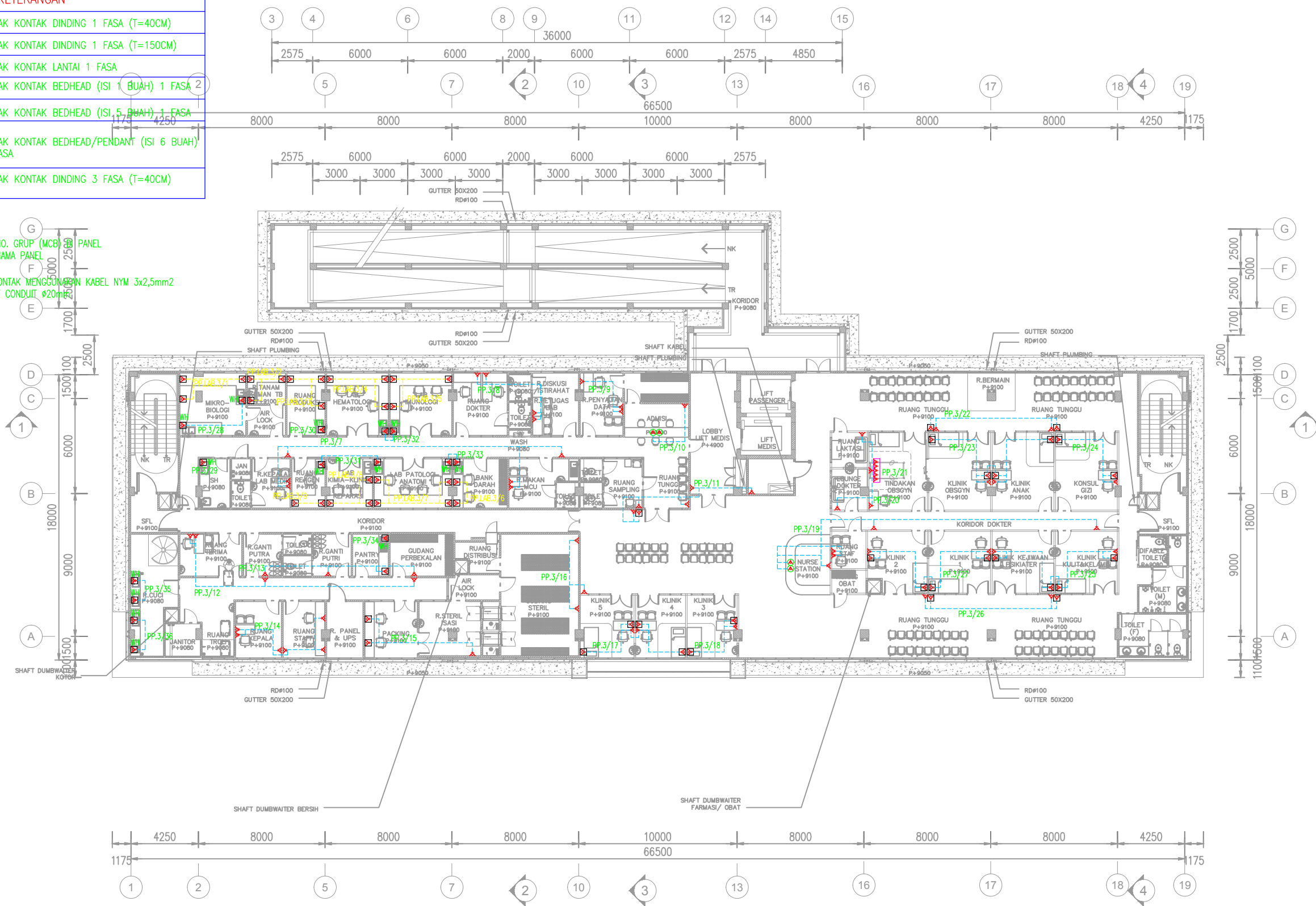
RUANG OK 2
 GRUP MCB :
 PPOK.4/1 = LAMPU RUANGAN
 PPOK.4/5 = LAMPU OPERASI
 PPOK.4/11 = PENDANT OK 1
 PPOK.4/17 = PENDANT OK 2

RUANG OK 1
 GRUP MCB :
 PPOK.4/1 = LAMPU RUANGAN
 PPOK.4/5 = LAMPU OPERASI
 PPOK.4/11 = PENDANT OK 1
 PPOK.4/17 = PENDANT OK 2

GS.4/1
 6 GANGS
 PP.4/4

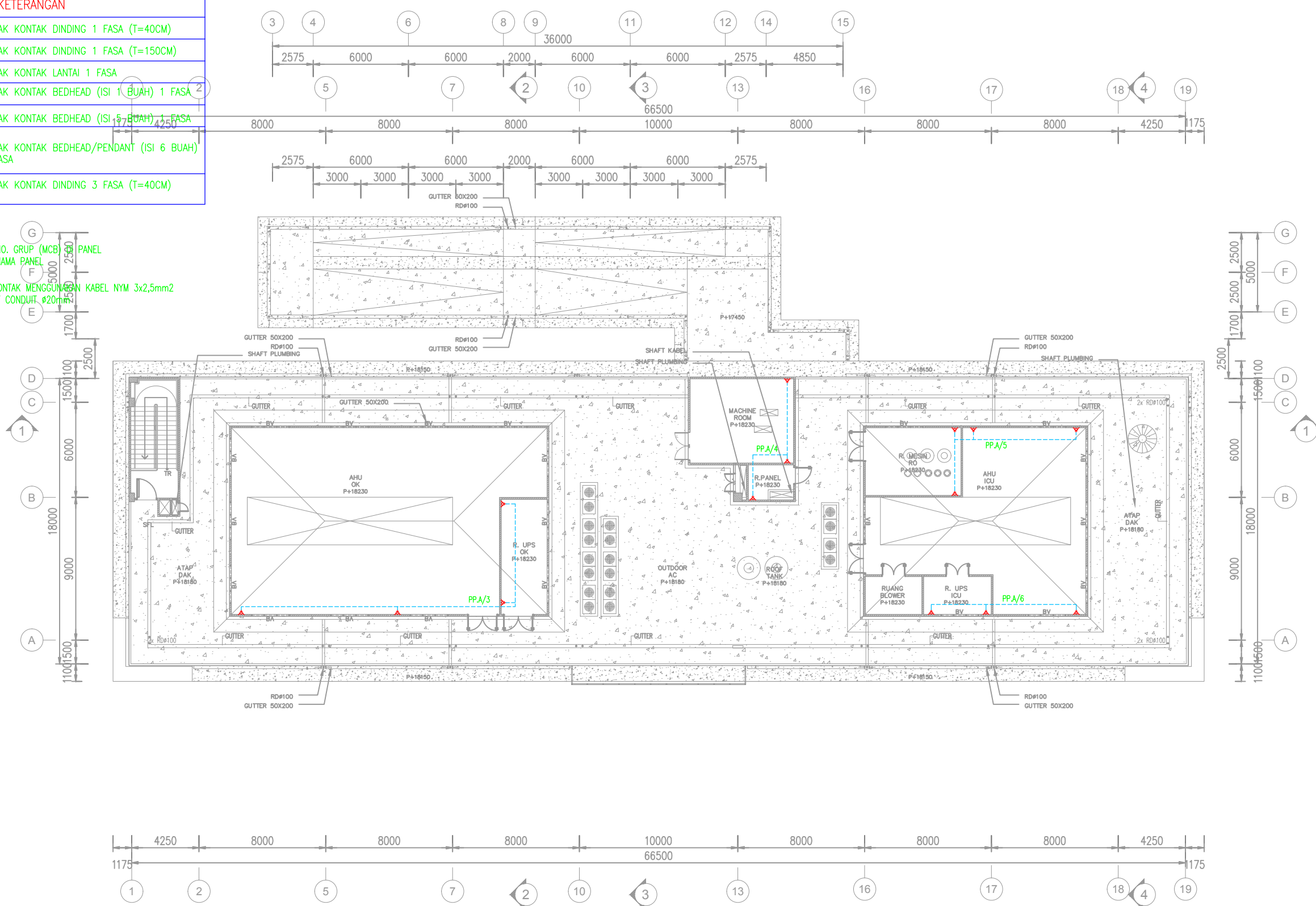
SIMBOL & KETERANGAN	
	KOTAK KONTAK DINDING 1 FASA (T=40CM)
	KOTAK KONTAK DINDING 1 FASA (T=150CM)
	KOTAK KONTAK LANTAI 1 FASA
	KOTAK KONTAK BEDHEAD (ISI 1 BUAH) 1 FASA
	KOTAK KONTAK BEDHEAD/PENDANT (ISI 6 BUAH) 1 FASA
	KOTAK KONTAK DINDING 3 FASA (T=40CM)

LP.X/X
 NO. GRUP (MCB) PANEL
 NAMA PANEL
 INSTALASI KOTAK KONTAK MENGGUNAKAN KABEL NYM 3x2,5mm²
 DALAM HIGH IMPACT CONDUIT Ø20mm



SIMBOL & KETERANGAN	
	KOTAK KONTAK DINDING 1 FASA (T=40CM)
	KOTAK KONTAK DINDING 1 FASA (T=150CM)
	KOTAK KONTAK LANTAI 1 FASA
	KOTAK KONTAK BEDHEAD (ISI 1 BUAH) 1 FASA
	KOTAK KONTAK BEDHEAD/PENDANT (ISI 6 BUAH) 1 FASA
	KOTAK KONTAK DINDING 3 FASA (T=40CM)

LP.X/X
 NO. GRUP (MCB) PANEL
 NAMA PANEL
 INSTALASI KOTAK KONTAK MENGGUNAKAN KABEL NYM 3x2,5mm²
 DALAM HIGH IMPACT CONDUIT Ø20mm



SIMBOL & KETERANGAN	
	IU : INDOOR UNIT/FAN COIL UNIT TYPE : SPLIT WALL MOUNTED
	IU : INDOOR UNIT/FAN COIL UNIT TYPE : CEILING CASSETTE
	OU : COMPRESSOR UNIT/OUTDOOR UNIT
IU.X-10	← NO. AC
1 PK	← KAPASITAS PENDINGINAN AC
PPAC.X-10	← URUTAN NOMOR PANEL AC
	PIPA REFRIGERANT AC
	KABEL POWER AC



- SHAFT PIPA REFRIGERANT AC
DI ATAS PLAFON
UK. 500x200mm
- PIPA REFRIGERANT AC
MENJAU KE OUTDOOR AC
LANTAI 2

- SHAFT PIPA REFRIGERANT AC
DI ATAS PLAFON
UK. 500x200mm
- PIPA REFRIGERANT AC
MENJAU KE OUTDOOR AC
LANTAI 2

- SHAFT PIPA REFRIGERANT AC
DI ATAS PLAFON
UK. 1000x200mm
- PIPA REFRIGERANT AC
MENJAU KE OUTDOOR AC
LANTAI 2

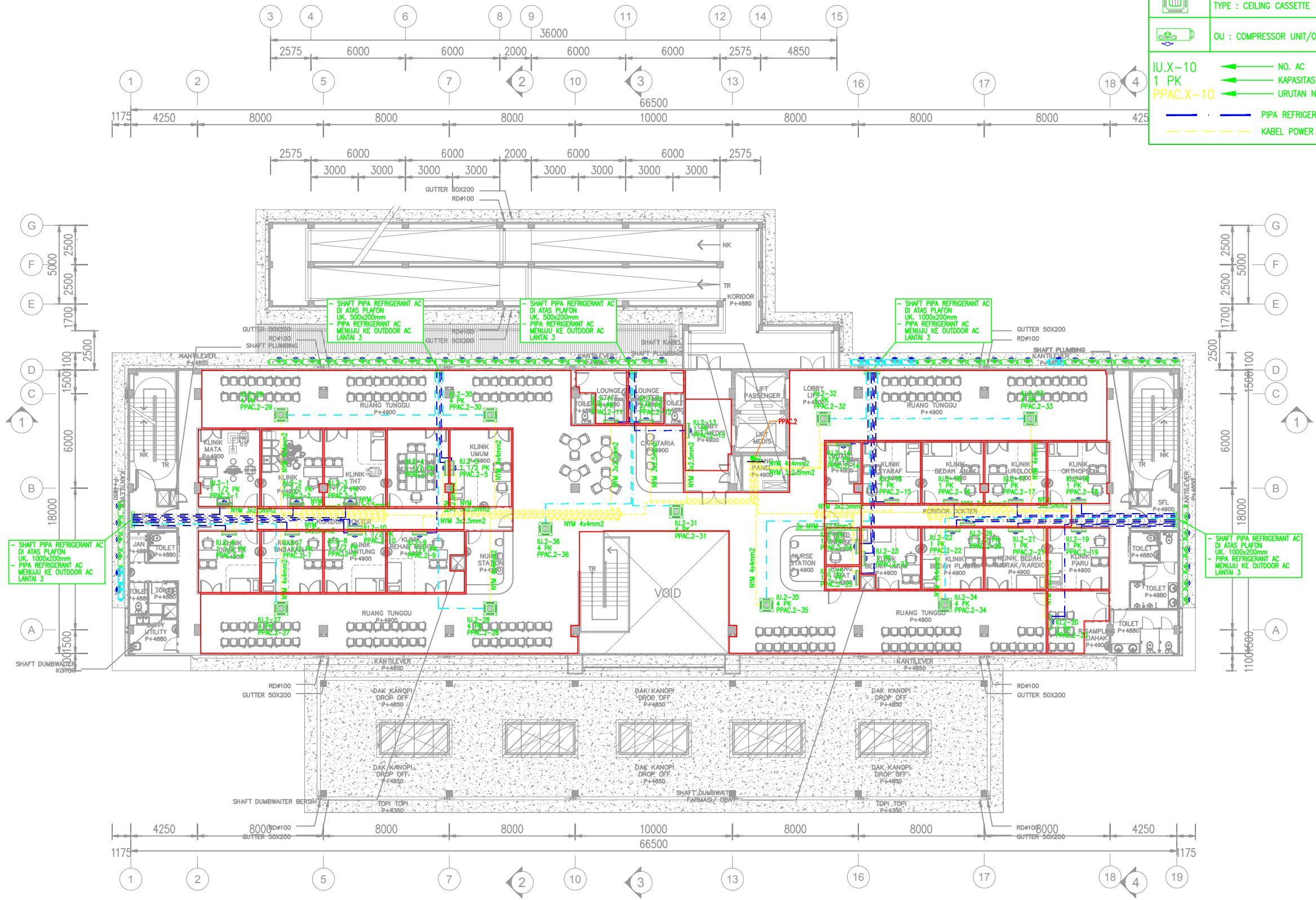
- SHAFT PIPA REFRIGERANT AC
DI ATAS PLAFON
UK. 500x200mm
- PIPA REFRIGERANT AC
MENJAU KE OUTDOOR AC
LANTAI 2

- SHAFT PIPA REFRIGERANT AC
DI ATAS PLAFON
UK. 1000x200mm
- PIPA REFRIGERANT AC
MENJAU KE OUTDOOR AC
LANTAI 2

- SHAFT PIPA REFRIGERANT AC
DI ATAS PLAFON
UK. 500x200mm
- PIPA REFRIGERANT AC
MENJAU KE OUTDOOR AC
LANTAI 2

PARKIR MOBIL
Kapasitas 83 mobil

SIMBOL & KETERANGAN	
	IU : INDOOR UNIT/FAN COIL UNIT TYPE : SPLIT WALL MOUNTED
	IU : INDOOR UNIT/FAN COIL UNIT TYPE : CEILING CASSETTE
	OU : COMPRESSOR UNIT/OUTDOOR UNIT
IU.X-10	← NO. AC
1 PK	← KAPASITAS PENDINGINAN AC
PPAC.X-10	← URUTAN NOMOR PANEL AC
	— PIPA REFRIGERANT AC
	— KABEL POWER AC



SHAF T PIPA REFRIGERANT AC DI ATAS PLAFON UK. 1000x200mm - PIPA REFRIGERANT AC MENULAU KE OUTDOOR AC LANTAI 3

SHAF T PIPA REFRIGERANT AC DI ATAS PLAFON UK. 500x200mm - PIPA REFRIGERANT AC MENULAU KE OUTDOOR AC LANTAI 3

SHAF T PIPA REFRIGERANT AC DI ATAS PLAFON UK. 1000x200mm - PIPA REFRIGERANT AC MENULAU KE OUTDOOR AC LANTAI 3

SHAF T PIPA REFRIGERANT AC DI ATAS PLAFON UK. 1000x200mm - PIPA REFRIGERANT AC MENULAU KE OUTDOOR AC LANTAI 3

SIMBOL & KETERANGAN	
	IU : INDOOR UNIT/FAN COIL UNIT TYPE : SPLIT WALL MOUNTED
	IU : INDOOR UNIT/FAN COIL UNIT TYPE : CEILING CASSETTE
	OU : COMPRESSOR UNIT/OUTDOOR UNIT
IU.X-10	← NO. AC
1 PK	← KAPASITAS PENDINGINAN AC
PPAC.X-10	← URUTAN NOMOR PANEL AC
	— PIPA REFRIGERANT AC
	- - - KABEL POWER AC

